

Slavko Vujević<sup>1</sup>, Zdenko Balaž<sup>2</sup> and Dino Lovrić<sup>1</sup>

<sup>1</sup>University of Split, Faculty of Electrical Engineering, Mechanical  
Engineering and Naval Architecture, Split, Croatia

<sup>2</sup>Croatian Motorways Ltd., Zagreb, Croatia

# **Ground Impedance of Cylindrical Metal Plate Buried in Homogeneous Earth**

## Introduction and brief outline of the paper

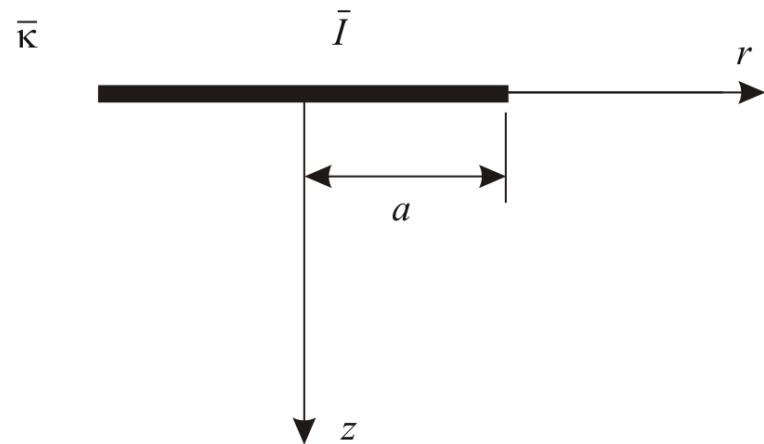
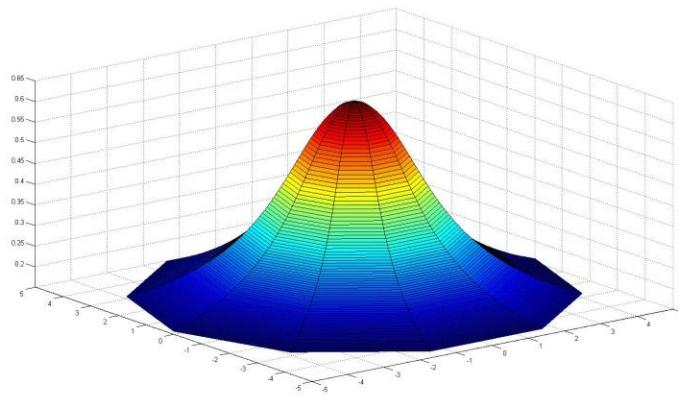
- cylindrical metal plates as grounding systems are usually used in ordinary households and offices
- plate ground impedance must be accurately computed (EMC applications, grounding analysis, ground fault current computation)
- ground impedance of plate buried in **homogeneous earth** will be derived using Galerkin-Bubnov weighted residual method
- combination of analytical and numerical integration will be used
- numerical examples

## Metal plate in homogeneous and unbounded medium

- scalar electric potential distribution of **equipotential** metal plate obtained by extending the expression derived by Koch to include A.C. effects

$$\bar{\phi} = \frac{\bar{I}}{j \cdot 8 \cdot \pi \cdot a \cdot \bar{\kappa}} \cdot \ell n \frac{\sqrt{r^2 + (|z| + j \cdot a)^2} + |z| + j \cdot a}{\sqrt{r^2 + (|z| - j \cdot a)^2} + |z| - j \cdot a}$$

$$\bar{\kappa} = \sigma + j \cdot 2 \cdot \pi \cdot f \cdot \epsilon_0 \cdot \epsilon_r$$



## Metal plate in homogeneous and unbounded medium

➤ due to numerical stability reasons practical to transform the expression into:

$$\bar{\varphi} = \frac{\bar{I}}{4 \cdot \pi \cdot a \cdot \bar{\kappa}} \cdot \tan^{-1} \frac{a}{\alpha} \quad \text{or} \quad \bar{\varphi} = \frac{\bar{I}}{4 \cdot \pi \cdot a \cdot \bar{\kappa}} \cdot \tan^{-1} \frac{\beta}{|z|}$$

$$\alpha = \alpha(a, r, z) = \sqrt{\frac{A + \sqrt{A^2 + 4 \cdot a^2 \cdot z^2}}{2}}$$
$$A = r^2 + z^2 - a^2$$

$$\beta = \beta(a, r, z) = \sqrt{\frac{-A + \sqrt{A^2 + 4 \cdot a^2 \cdot z^2}}{2}}$$

## Metal plate in homogeneous and unbounded medium

- metal plate potential can be obtained by introducing  $r = 0$  and  $z = 0$  into

$$\bar{\Phi} = \frac{\bar{I}}{4 \cdot \pi \cdot a \cdot \bar{\kappa}} \cdot \tan^{-1} \frac{a}{\alpha(a, r, z)}$$

- metal plate potential:

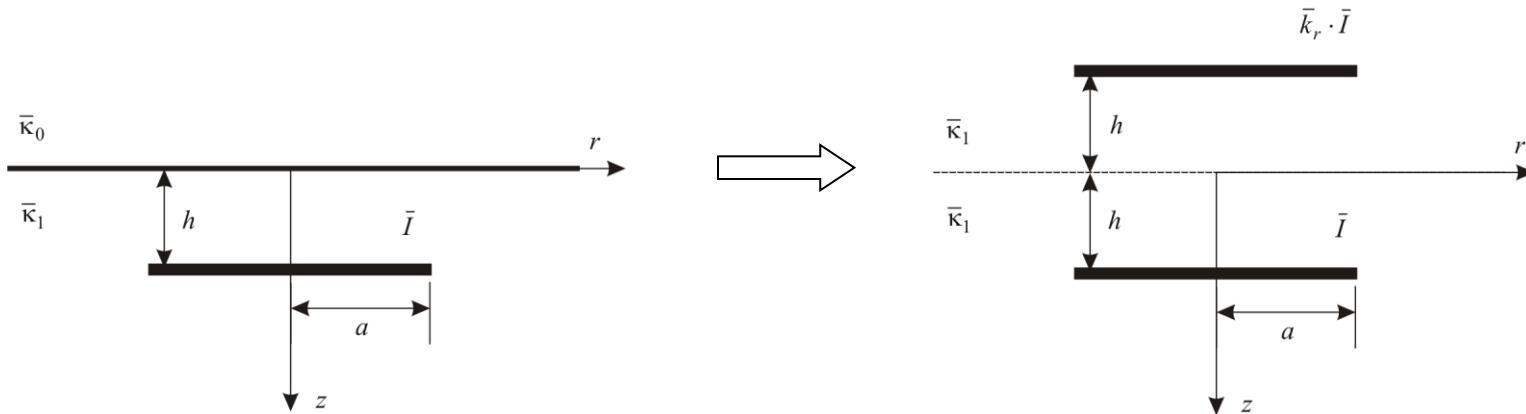
$$\bar{\Phi}_{pu} = \frac{\bar{I}}{8 \cdot a \cdot \bar{\kappa}}$$

- metal plate ground impedance in **homogeneous and unbounded** medium:

$$\bar{Z}_{pu} = \frac{1}{8 \cdot a \cdot \bar{\kappa}}$$

## Metal plate in homogeneous earth

- two-layer medium is observed consisting of air and homogeneous earth



- scalar electric potential in homogeneous earth:

$$\begin{aligned}\bar{\varphi} = & \frac{\bar{I}}{4 \cdot \pi \cdot a \cdot \bar{\kappa}_1} \cdot \tan^{-1} \frac{a}{\alpha(a, r, z-h)} \\ & + \frac{\bar{k}_r \cdot \bar{I}}{4 \cdot \pi \cdot a \cdot \bar{\kappa}_1} \cdot \tan^{-1} \frac{a}{\alpha(a, r, z+h)}\end{aligned}$$

$$\bar{k}_r = \frac{\bar{\kappa}_1 - \bar{\kappa}_0}{\bar{\kappa}_1 + \bar{\kappa}_0}$$

## Metal plate in homogeneous earth

- physically constant metal plate potential  $\bar{\Phi}_p$  is approximated using Galerkin-Bubnov weighted residual method

$$\iint_{S_p} (\bar{\varphi}_p - \bar{\Phi}_p) \cdot N \cdot dS = 0 \quad N - \text{shape/weighting function}$$

- shape function  $N$  is derived from the surface current density of a plate which leaks in homogeneous unbounded medium from both sides of the plate

$$\bar{J} = -2 \cdot \bar{\kappa} \cdot \lim_{\substack{|z| \rightarrow 0 \\ r \leq a}} \frac{\partial \varphi}{\partial z} \quad \longrightarrow \quad \bar{J} = \frac{\bar{I}}{2 \cdot \pi \cdot a \cdot \sqrt{a^2 - r^2}} = N \cdot \bar{I}$$

## Metal plate in homogeneous earth

- approximation of the constant metal plate potential:

$$\overline{\Phi}_p = \iint_{S_p} \overline{\Phi}_p \cdot N \cdot dS = 0$$

- scalar potential for  $z = h$  and  $r \leq a$ :

$$\overline{\Phi}_p = \overline{P}(a, r, 0) \cdot \bar{I} + \overline{P}_m(a, r, 2 \cdot h) \cdot \bar{I}$$

$$\overline{P}(a, r, 0) = \frac{1}{4 \cdot \pi \cdot a \cdot \bar{\kappa}_1} \cdot \tan^{-1} \frac{a}{\alpha(a, r, 0)} = \frac{1}{8 \cdot a \cdot \bar{\kappa}_1}$$

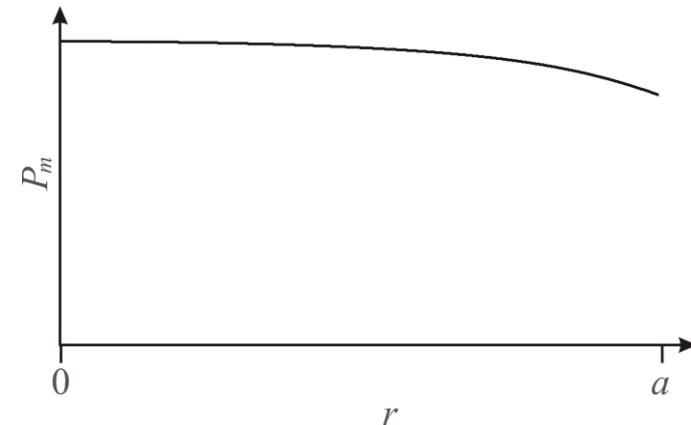
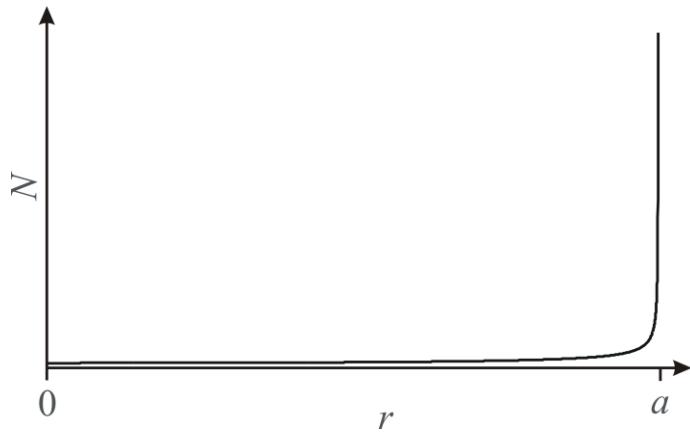
$$\overline{P}_m(a, r, 2 \cdot h) = \frac{\bar{k}_r}{4 \cdot \pi \cdot a \cdot \bar{\kappa}_1} \cdot \tan^{-1} \frac{a}{\alpha(a, r, 2 \cdot h)}$$

## Metal plate in homogeneous earth

- approximation of the constant metal plate potential:

$$\bar{\Phi}_p = \bar{I} \cdot \left[ \frac{1}{8 \cdot a \cdot \bar{\kappa}_1} + \int_0^a N \cdot \bar{P}_m(a, r, 2 \cdot h) \cdot 2 \cdot \pi \cdot r \cdot dr \right]$$

- combination of analytical and five-point Gaussian numerical integration



## Metal plate in homogeneous earth

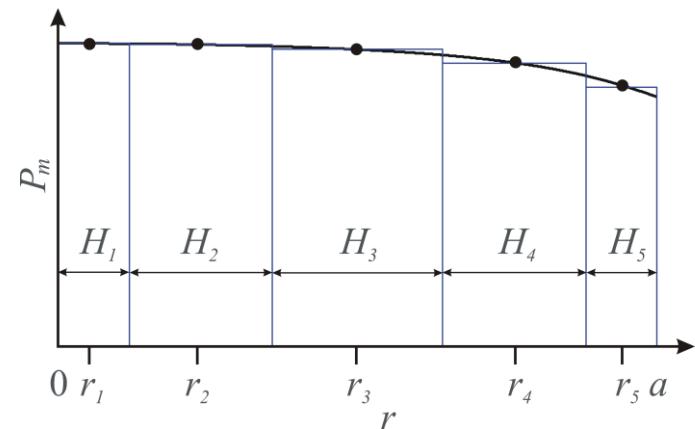
➤ combined integration yields

$$\bar{Z}_{mu} = \sum_{j=1}^5 \bar{P}_m(a, r_j, 2 \cdot h) \cdot W_j$$

$$r_j = u_j \cdot a$$

$$W_j = \int_{r_{sj}}^{r_{ej}} N \cdot 2 \cdot \pi \cdot r \cdot dr$$

$$= \sqrt{1 - \left(\frac{r_{sj}}{a}\right)^2} - \sqrt{1 - \left(\frac{r_{ej}}{a}\right)^2}$$



$j$	Coordinates $u_j$	Weights $H_j$
1	$\frac{1}{2} - \frac{1}{6} \cdot \sqrt{5+2 \cdot \sqrt{\frac{10}{7}}}$	$\frac{322 - 13 \cdot \sqrt{70}}{1800}$
2	$\frac{1}{2} - \frac{1}{6} \cdot \sqrt{5-2 \cdot \sqrt{\frac{10}{7}}}$	$\frac{322 + 13 \cdot \sqrt{70}}{1800}$
3	$\frac{1}{2}$	$\frac{64}{225}$
4	$\frac{1}{2} + \frac{1}{6} \cdot \sqrt{5-2 \cdot \sqrt{\frac{10}{7}}}$	$\frac{322 + 13 \cdot \sqrt{70}}{1800}$
5	$\frac{1}{2} + \frac{1}{6} \cdot \sqrt{5+2 \cdot \sqrt{\frac{10}{7}}}$	$\frac{322 - 13 \cdot \sqrt{70}}{1800}$

## Metal plate in homogeneous earth

- final expression for plate ground impedance in homogeneous earth:

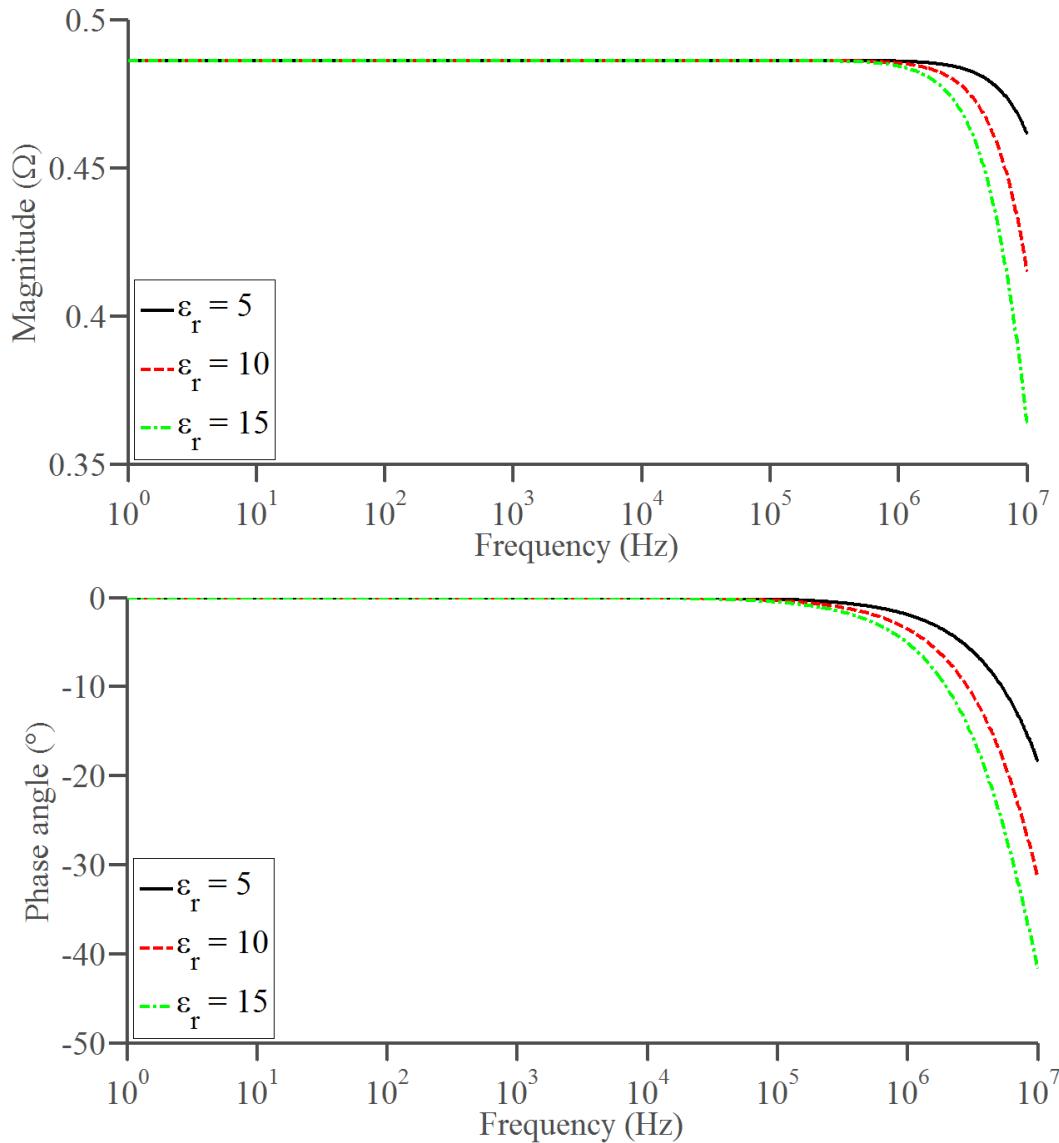
$$\bar{Z}_p = \frac{1}{8 \cdot a \cdot \bar{\kappa}_1} + \sum_{j=1}^5 \bar{P}_m(a, r_j, 2 \cdot h) \cdot W_j$$

- high accuracy and robustness achieved by analytically integrating the weighting function  $N$  which has a singularity at  $r = a$
- easily extended to compute mutual impedances between different plates

## Numerical examples

- metal plate of radius  $a = 50$  m buried at depth  $h = 1$  m is observed
- three types of earth with respect to conductivity observed:
  - high conductivity earth ( $0.01$  S/m  $\leftrightarrow$   $100$   $\Omega\text{m}$ )
  - medium conductivity earth ( $0.001$  S/m  $\leftrightarrow$   $1\ 000$   $\Omega\text{m}$ )
  - low conductivity earth ( $0.0001$  S/m  $\leftrightarrow$   $10\ 000$   $\Omega\text{m}$ )
- three types of earth with respect to relative permittivity observed:
  - $\epsilon_r = 5$
  - $\epsilon_r = 10$
  - $\epsilon_r = 15$

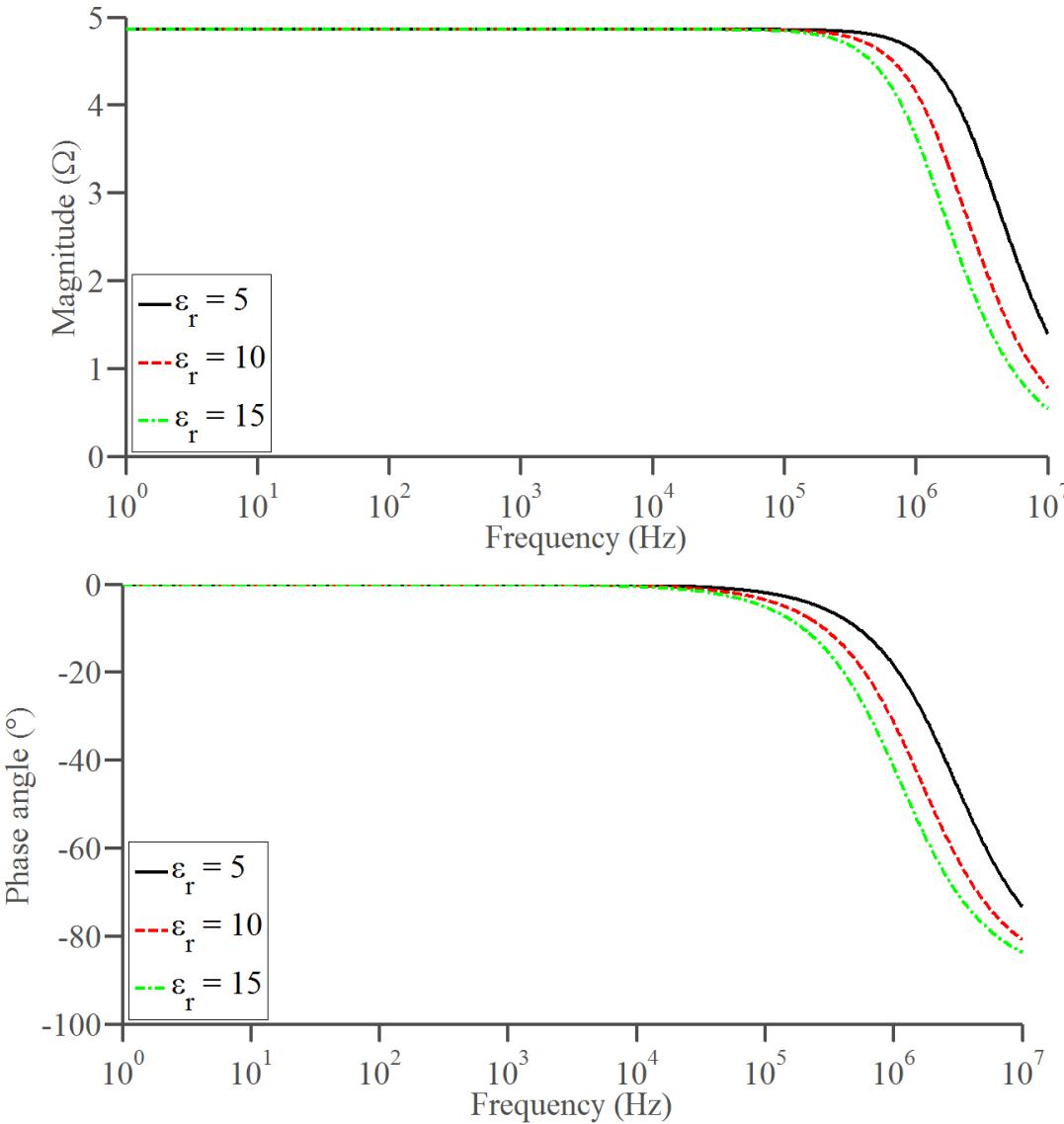
## High conductivity earth



$$\bar{Z}_p = Z_p \cdot e^{j \cdot \phi_p}$$

- magnitude starts to decay at high frequencies (1 MHz)
- phase angle tends to  $-90^\circ$  at high frequencies
- ground impedance becomes capacitive at high frequencies
- decrease more pronounced for higher permittivity values

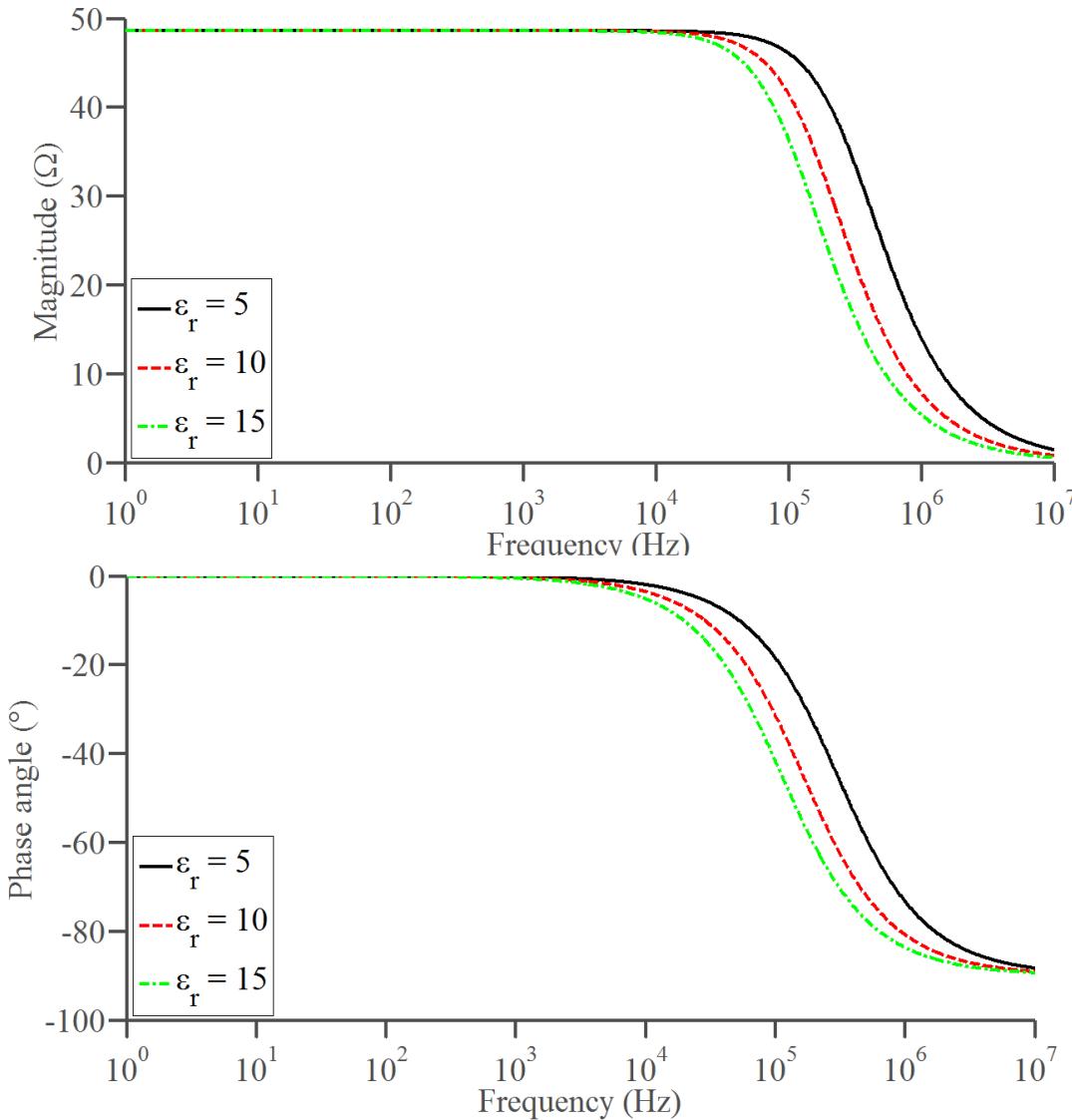
## Medium conductivity earth



$$\bar{Z}_p = Z_p \cdot e^{j \cdot \phi_p}$$

- magnitude starts to decay for  $f \geq 100$  kHz
- ground impedance becomes capacitive at lower frequencies

## Low conductivity earth



$$\bar{Z}_p = Z_p \cdot e^{j \cdot \varphi_p}$$

- magnitude starts to decay for  $f \geq 10$  kHz
- capacitive character of ground impedance even lower frequencies

## Summary

- highly accurate and robust algorithm for ground impedance of equipotential metal plate in homogeneous earth developed
- this is achieved by analytically integrating the weighting function  $N$  which has a singularity at  $r = a$
- algorithm can be easily extended to obtain mutual impedances between different plates
- future research: extension of algorithm to accommodate a horizontal multilayer medium by the use of more sophisticated imaging methods

Thank you!